

# Optimization of elastic circular plates with additional supports

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- Mroz, Rozvany (1975)
- Akesson, Olhoff (1988)

# Annular plate

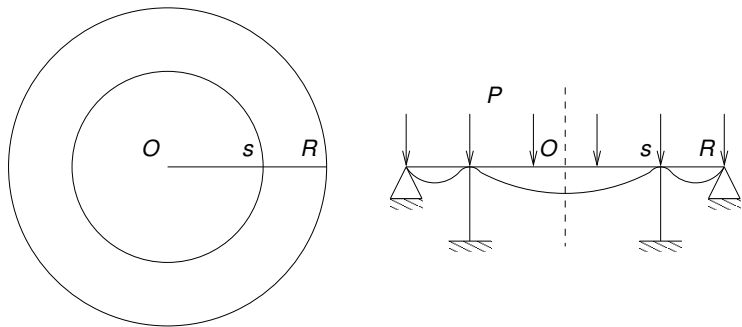


Figure: A circular plate with support.

$$J = \int_0^R W^k r dr + \mu_0 2\pi s \quad (1)$$

The aim of the paper is to determine the design of the plate with an additional support which minimizes the cost function (1) so that at each value of  $P$  governing equations of the theory of thin axisymmetric plates with appropriate boundary conditions are satisfied.

- Equilibrium conditions

$$\frac{d}{dr}(rM_1) - M_2 - rQ = 0, \quad \frac{d}{dr}(rQ) = -Pr$$

- Strain components

$$\kappa_1 = -\frac{d^2W}{dr^2}, \quad \kappa_2 = -\frac{1}{r} \frac{dW}{dr}$$

- Hooke's law

$$M_1 = D(\kappa_1 + \nu\kappa_2), \quad M_2 = D(\kappa_2 + \nu\kappa_1)$$

$$D = \frac{Eh^3}{12(1 - \nu^2)}$$

- Governing equations

$$\begin{aligned}\frac{dW}{dr} &= Z, \\ \frac{dZ}{dr} &= -\frac{M_1}{D} - \frac{\nu Z}{r}, \\ \frac{dM_1}{dr} &= \frac{D(\nu^2 - 1)Z}{r^2} - \frac{M_1(1 - \nu)}{r} + Q, \\ \frac{dQ}{dr} &= -\frac{Q}{r} - P(r).\end{aligned}\tag{2}$$

- Boundary conditions

$$M_1(R) = 0, \quad W(R) = 0 \quad (3)$$

$$\frac{dW}{dr}(0) = 0, \quad Q(0) = 0 \quad (4)$$



$$J_* = \mu s + \int_0^s F_* dr + \int_s^R F_* dr \quad (5)$$

$$\begin{aligned} F_* = & W^k + \psi_1 \left( \frac{dW}{dr} - Z \right) + \psi_2 \left( \frac{dZ}{dr} + \frac{M_1}{D} + \frac{\nu Z}{r} \right) + \\ & + \psi_3 \left( \frac{dM_1}{dr} - \frac{D(\nu^2 - 1)Z}{r^2} + \frac{M_1(1 - \nu)}{r} - Q \right) + \\ & + \psi_4 \left( \frac{dQ}{dr} + \frac{Q}{r} + P(r) \right) \end{aligned} \quad (6)$$

$$\psi_2(s-0) - \psi_2(s+0) = 0,$$

$$\psi_3(s-0) - \psi_3(s+0) = 0, \quad (7)$$

$$\psi_4(s-0) = \psi_4(s+0) = 0,$$

$$\mu + [\psi_1(s)] \frac{dW(s)}{dr} + \psi_3(s) \left[ \frac{dM_1(s)}{dr} \right] = 0. \quad (8)$$

$$\psi_1(0) = 0, \quad \psi_3(0) = 0 \quad (9)$$

$$\psi_2(R) = 0, \quad \psi_4(R) = 0 \quad (10)$$

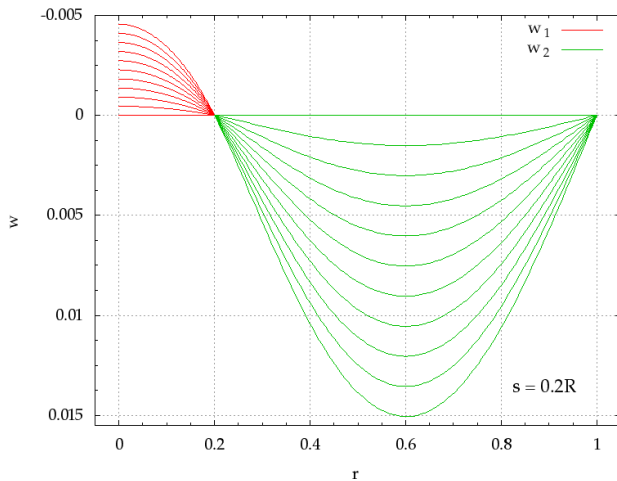
$$\begin{aligned}\frac{d\psi_1}{dr} &= rkW^{k-1}, \\ \frac{d\psi_2}{dr} &= -\psi_1 + \frac{\nu\psi_2}{r} - \frac{D(\nu^2 - 1)\psi_3}{r^2}, \\ \frac{d\psi_3}{dr} &= \frac{\psi_2}{D} + \frac{\psi_3(1 - \nu)}{r}, \\ \frac{d\psi_4}{dr} &= -\psi_3 + \frac{\psi_4}{r}.\end{aligned}\tag{11}$$

$$\begin{aligned}W &= \frac{Pr^4}{64D} + A_{1j}r^2 \ln r + A_{2j}r^2 + A_{3j} \ln r + A_{4j}, \\Z &= \frac{Pr^3}{16D} + A_{1j}r(2 \ln r + 1) + 2A_{2j}r + \frac{A_{3j}}{r}, \\M_1 &= -\frac{Pr^2(3 + \nu)}{16} - A_{1j}D[3 + \nu + 2(1 + \nu) \ln r] - \\&\quad - 2DA_{2j}(1 + \nu) - \frac{D(\nu - 1)}{r^2}A_{3j}, \\M_2 &= -\frac{Pr^2(1 + 3\nu)}{16} - A_{1j}D[1 + 3\nu + 2(1 + \nu) \ln r] - \\&\quad - 2DA_{2j}(1 + \nu) - \frac{D(\nu - 1)}{r^2}A_{3j}.\end{aligned}\tag{12}$$

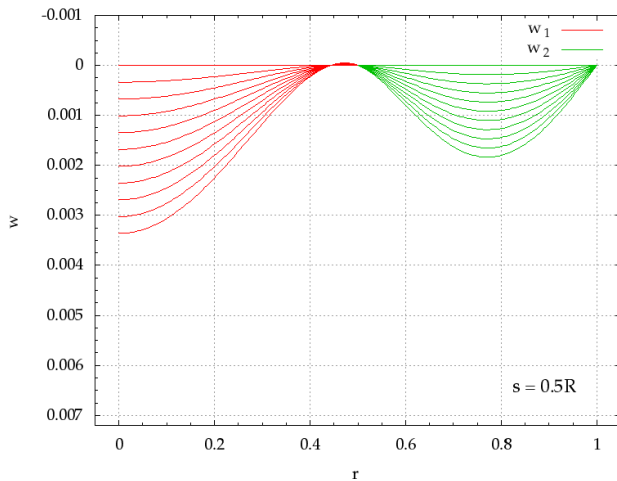
## Solution of the adjoint system

$$\begin{aligned}\psi_1 &= \frac{r^2}{2} + C_{1j}, \\ \psi_2 &= C_{2j} + \frac{C_{3j}}{r} - \frac{(3 + \nu)r^3}{16} - \frac{C_{1j}(1 + \nu)r \ln r}{2}, \\ \psi_3 &= \frac{C_{2j}r^2}{D(\nu + 1)} + \frac{C_{3j}}{D(\nu - 1)} - \frac{r^4}{16D} - \\ &\quad - \frac{C_{1j}r^2}{D(\nu^2 - 1)} + \frac{C_{1j}r^2[(1 - \nu) \ln r + 1]}{2D(\nu - 1)}, \\ \psi_4 &= -\frac{C_{2j}r^3}{2D(\nu + 1)} - \frac{C_{3j}r \ln r}{D(\nu - 1)} + C_{4j}r + \\ &\quad + \frac{r^5}{64D} + \frac{C_{1j}r^3 \ln r}{4D} + \frac{C_{1j}(3 - 2\nu - \nu^2)r^3}{8D(\nu^2 - 1)}\end{aligned}\tag{13}$$

# Deflection

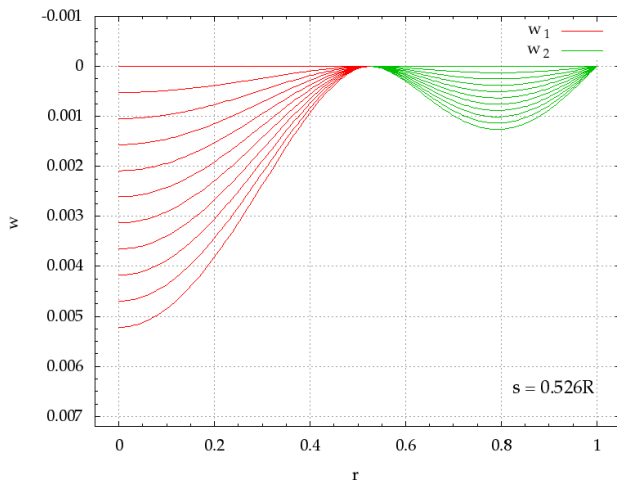


# Deflection

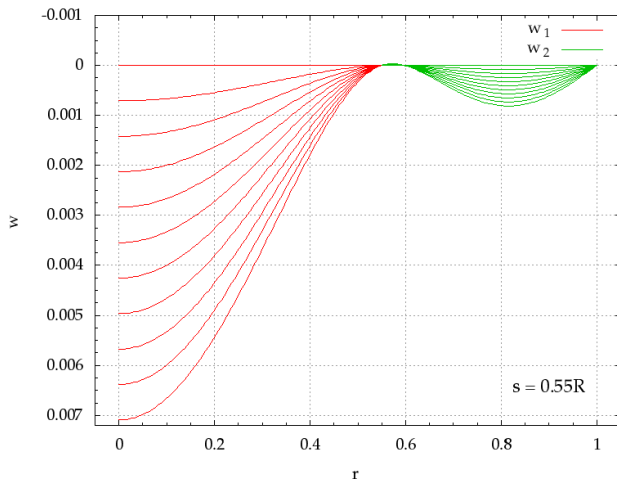




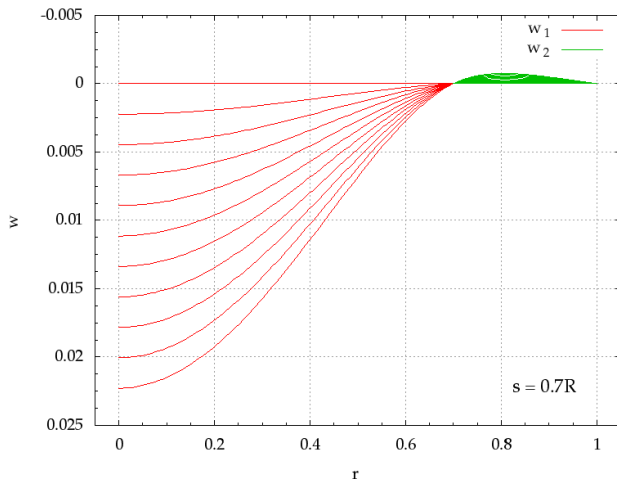
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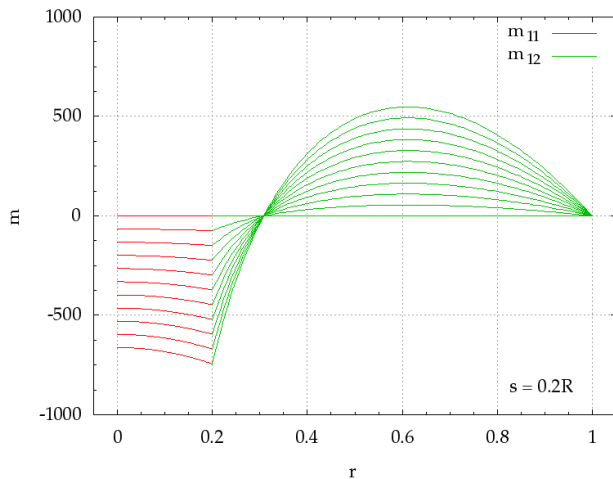
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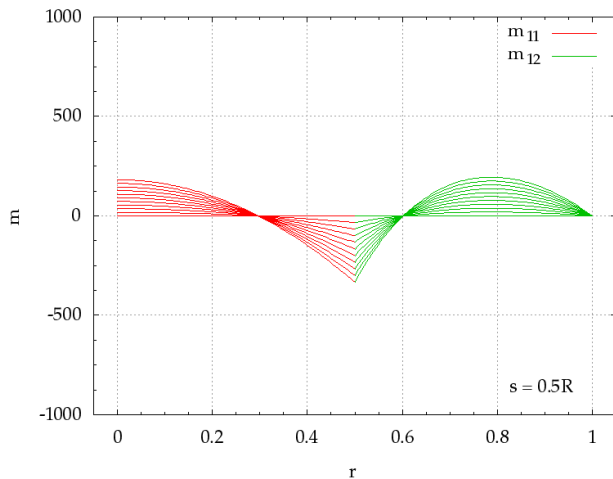
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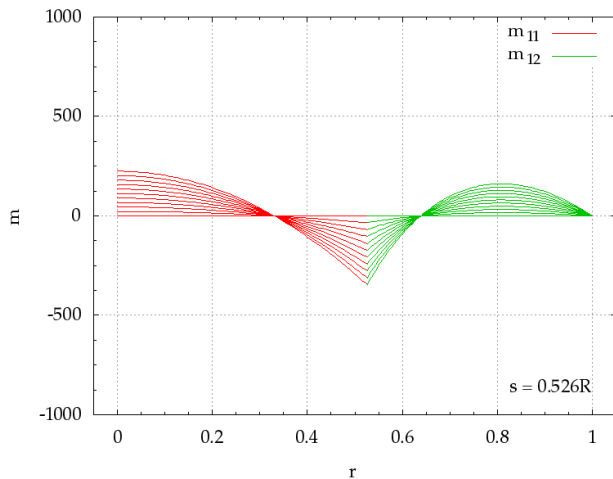
# Moment



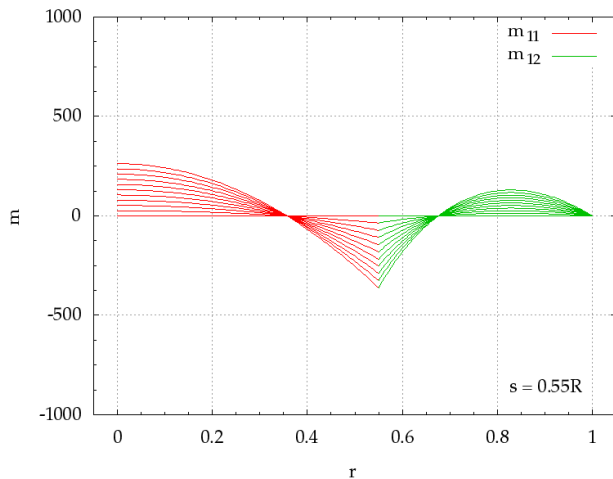
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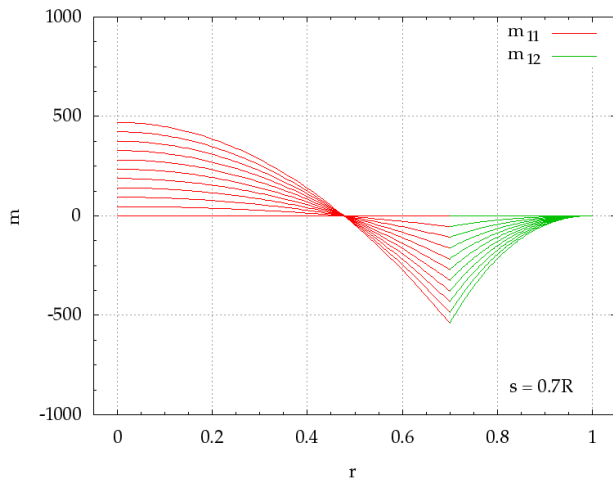
# Moment



# Moment

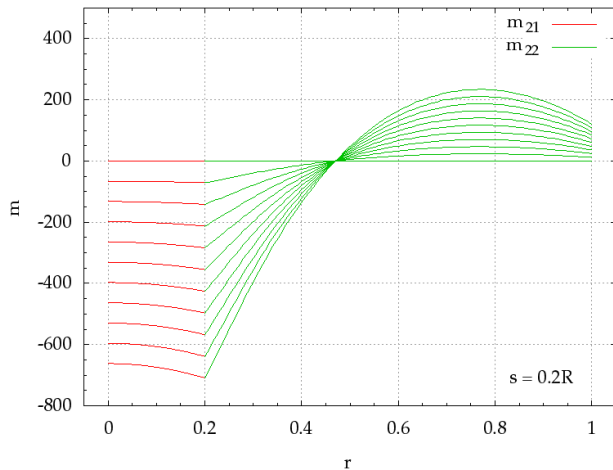


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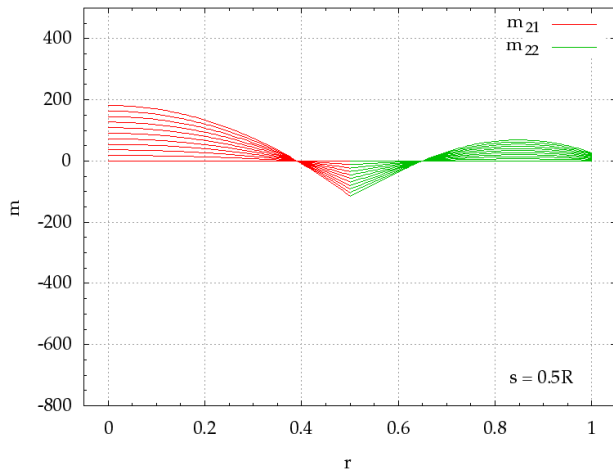




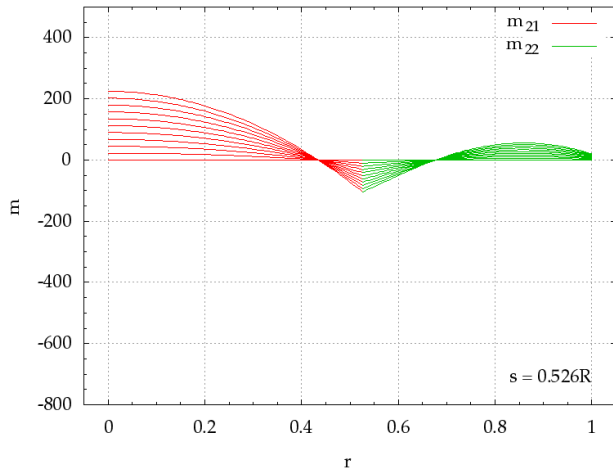
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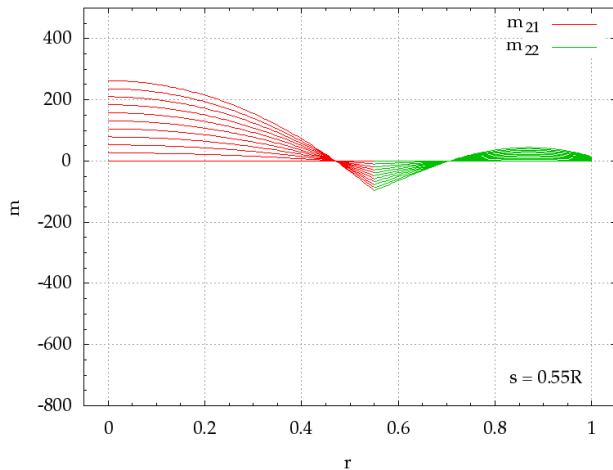
# Moment



# Moment



# Moment



# Moment

